# PVT Measurements on Fullerite from 30 to $330{ }^{\circ} \mathrm{C}$ and at Pressures to 200 MPa 

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#### Abstract

Specific volumes of $\mathrm{C}_{60} / \mathrm{C}_{70}$ (3:1) fullerites are measured up to $330^{\circ} \mathrm{C}$ and 200 MPa using a dilatometer-type PVT (pressure-volume-temperature) apparatus. The compressibility and thermal expansion of fullerites are found to be much higher than those of graphite. This is consistent with a lower degree of molecular and supermolecular (crystal) packing in fullerites compared to graphite.


## Introduction

Fullerene molecules (bucky balls) are ball-like cage analogues of carbon. Their molecular packing and crystal packing (e.g., face-centered cubic (fcc) for $\mathrm{C}_{60}$ ) are less dense than those of graphite and diamond. This is consistent with the difference in density between fullerites and graphite or diamond. Here we use the term "fullerenes" for the molecules, and "fullerites" for the solids. For example, the densities of graphite and diamond are 2.267 and $3.515 \mathrm{~g} \cdot \mathrm{~cm}^{-3}$ at $20^{\circ} \mathrm{C}$, respectively (1), while the density of $\mathrm{C}_{60}$ is only $1.65 \mathrm{~g} \cdot \mathrm{~cm}^{-3}$ $(2,3)$. Larger fullerites are even less dense ( 2,3 ). This is because there is more free volume between the cages and inside the cages. Therefore, the compressibility and thermal expansion of such materials are expected to be much higher than those of graphite and diamond, which are known to be very low. This is consistent with the isothermal bulk modulus of $K / \mathrm{GPa}=18.1+5.7 P /$ GPa determined by Duclos et al. (4) on the basis of the ambient-temperature compressibilities of $\mathrm{C}_{60}$ fullerite up to 20 GPa . Also, Fischer and co-workers (5) report that the ambient-temperature volume compressibility of solid $\mathrm{C}_{60}$ is $7.0 \times 10^{-5} \mathrm{MPa}^{-1}$, which is 3 and 40 times greater than those of graphite and diamond, respectively.

However, there is a solid-solid phase transition (simple cubic to face-centered cubic) for $\mathrm{C}_{60}$ at $-13{ }^{\circ} \mathrm{C}$ at ambient pressure ( 6,7 ), which shifts to higher temperatures with increasing pressure at a rate of $0.117 \mathrm{~K} \cdot \mathrm{MPa}^{-1}$, as measured by Kriza and co-workers (8). This means that, above 350 MPa at ambient temperatures, the phase structure (crystal form) of $\mathrm{C}_{60}$ fullerite is different from that at lower pressure. Therefore, the volume changes resulting from changes in pressure have a contribution from the phase transition (similar to melting expansion), in addition to the compressibility contribution. This may indicate that there is a significant error in the results of Fischer and co-workers (5).
High-pressure IR spectra $(9,10)$ show that intramolecular vibrations shift with increasing pressure, due to the reduction in intermolecular distance. Furthermore, the frequency shifts are found to be reversible up to 3200 MPa , which suggests that the fullerene cages do not collapse and rearrange themselves below 3200 MPa .
Thus, further measurements on the compressibility, expansivity, and phase behavior of fullerites at both elevated temperature and pressure are necessary. It is the objective of this report to determine the fullerite compressibility and phase behavior at higher temperatures from high-pressure, high-temperature PVT data, and to compare them to those of graphite.

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Fullerite
Graphite
Figure 1. Photographs of fullerite and graphite cylinders.

## Experimental Section

Fullerites used in this work are prepared by the carbon electrical arcing technique, and isolated by toluene extraction. The samples contain about $75 \mathrm{~mol} \% \mathrm{C}_{60}$ and $25 \mathrm{~mol} \% \mathrm{C}_{70}$ as determined by high-resolution ${ }^{13} \mathrm{C}$ NMR. Graphite is a spectroscopy grade powder (SP-1) from Union Carbide. Sample powders are dried under vacuum at $100^{\circ} \mathrm{C}$ for 24 h . Cylindrical samples (diameter 10.0 mm ) are formed in a SPECAC die by slowly applying a total force of 2500 kg over a cross-section of $0.785 \mathrm{~cm}^{2}(P \approx 315 \mathrm{MPa})$ under vacuum. The densities of the cylinders are estimated from their lengths and diameters measured with a micrometer) and their masses (measured with an analytical balance).

Pressure-volume-temperature (PVT) properties of fullerites and graphite are determined in a dilatometer-type PVT apparatus (11) manufactured by Gnomix, Inc. (Boulder, CO). A cylindrical sample with a total volume of about $1 \mathrm{~cm}^{3}$ is placed in a chamber with a flexible bellows. The volume in the chamber not taken by the sample is filled with mercury, after evacuation to $4-\mathrm{kPa}$ vacuum. Isothermal compression experiments are conducted in the temperature range of $30-$ $350^{\circ} \mathrm{C}$ and pressure range of $10-200 \mathrm{MPa}$, and extrapolated to 0 MPa . The temperature interval is $20^{\circ} \mathrm{C}$, and the residence time at each pressure is 60 s . The manufacturerquoted accuracy is $0.001-0.002 \mathrm{~cm}^{3} \cdot \mathrm{~g}^{-1}$, but the resolution is about 10 times better.

## Results and Discussion

Pictures of the compressed fullerite and graphite samples are shown in Figure 1. The fullerite density, $d_{f}$, is found to be $1.58 \mathrm{~g} \cdot \mathrm{~cm}^{-3}$, and the graphite density, $d_{\mathrm{g}}$, is found to be $2.15 \mathrm{~g} \cdot \mathrm{~cm}^{-3}$, at ambient conditions. These values are close to the literature values of 1.65 and $2.267 \mathrm{~g} \cdot \mathrm{~cm}^{-3}$, respectively (1-3), which is our test for achieving good, void-free samples for subsequent PVT experiments.

PVT results for fullerites given in Table 1 and plotted in

Table 1. Isothermal PVT Results for $C_{60} / C_{70}(3: 1)$ Fullerites ( $V_{0}=0.632 \mathrm{~cm}^{3} \cdot{ }^{-1}$ at $25{ }^{\circ} \mathrm{C}$ and 0.1 MPa , Specific Volume at Given $t$ and $P$ is $V_{0}+\Delta V$ )

| $t /{ }^{\circ} \mathrm{C}$ | $P / \mathrm{MPa}$ | $\Delta V /\left(\mathrm{cm}^{3} \cdot \mathrm{~g}^{-1}\right)$ | $t /{ }^{\circ} \mathrm{C}$ | $P / \mathrm{MPa}$ | $\Delta V /\left(\mathrm{cm}^{3} \cdot \mathrm{~g}^{-1}\right)$ | $t /{ }^{\circ} \mathrm{C}$ | $P / \mathrm{MPa}$ | $\Delta V /\left(\mathrm{cm}^{8} \cdot \mathrm{~g}^{-1}\right)$ | $t /{ }^{\circ} \mathrm{C}$ | $P / \mathrm{MPa}$ | $\Delta V /\left(\mathrm{cm}^{3} \cdot \mathrm{~g}^{-1}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30.0 | 0 | 0.0017 | 110.9 | 0 | 0.0042 | 191.0 | 0 | 0.0201 | 270.1 | 0 | 0.0389 |
| 30.0 | 10 | 0.0002 | 110.9 | 10 | 0.0031 | 191.1 | 10 | 0.0182 | 270.2 | 10 | 0.0349 |
| 30.0 | 20 | -0.0015 | 111.2 | 20 | 0.0020 | 191.6 | 20 | 0.0165 | 271.1 | 20 | 0.0311 |
| 29.8 | 30 | -0.0028 | 111.4 | 30 | 0.0009 | 191.7 | 30 | 0.0147 | 271.7 | 30 | 0.0279 |
| 29.9 | 40 | -0.0038 | 111.5 | 40 | -0.0003 | 191.7 | 40 | 0.0130 | 272.0 | 40 | 0.0253 |
| 30.0 | 50 | -0.0048 | 111.6 | 50 | -0.0014 | 191.7 | 50 | 0.0115 | 272.3 | 50 | 0.0228 |
| 30.0 | 60 | -0.0058 | 111.7 | 60 | -0.0023 | 191.7 | 60 | 0.0100 | 272.4 | 60 | 0.0207 |
| 30.0 | 70 | -0.0068 | 111.8 | 70 | -0.0033 | 191.9 | 70 | 0.0086 | 272.5 | 70 | 0.0187 |
| 29.9 | 80 | -0.0077 | 112.0 | 80 | -0.0042 | 192.1 | 80 | 0.0072 | 272.8 | 80 | 0.0168 |
| 29.9 | 90 | -0.0086 | 112.1 | 90 | -0.0051 | 192.2 | 90 | 0.0059 | 272.9 | 90 | 0.0152 |
| 29.8 | 100 | -0.0095 | 112.2 | 100 | -0.0060 | 192.5 | 100 | 0.0045 | 273.2 | 100 | 0.0137 |
| 29.9 | 110 | -0.0103 | 112.3 | 110 | -0.0069 | 192.6 | 110 | 0.0034 | 273.6 | 110 | 0.0121 |
| 29.9 | 120 | -0.0112 | 112.3 | 120 | -0.0077 | 192.9 | 120 | 0.0021 | 273.7 | 120 | 0.0107 |
| 30.0 | 130 | -0.0119 | 112.2 | 130 | -0.0084 | 193.1 | 130 | 0.0009 | 273.7 | 130 | 0.0093 |
| 30.0 | 140 | -0.0127 | 112.3 | 140 | -0.0091 | 193.4 | 140 | -0.0002 | 273.7 | 140 | 0.0081 |
| 30.0 | 150 | -0.0134 | 112.3 | 150 | -0.0099 | 193.6 | 150 | -0.0013 | 273.8 | 150 | 0.0068 |
| 29.9 | 160 | -0.0141 | 112.3 | 160 | -0.0106 | 193.8 | 160 | -0.0025 | 274.0 | 160 | 0.0056 |
| 29.9 | 170 | -0.0148 | 112.3 | 170 | -0.0113 | 194.0 | 170 | -0.0035 | 274.1 | 170 | 0.0044 |
| 29.9 | 180 | -0.0155 | 112.3 | 180 | -0.0121 | 194.1 | 180 | -0.0045 | 274.3 | 180 | 0.0034 |
| 29.9 | 190 | -0.0162 | 112.4 | 190 | -0.0127 | 194.3 | 190 | -0.0055 | 274.5 | 190 | 0.0023 |
| 29.9 | 200 | -0.0168 | 112.3 | 200 | -0.0134 | 194.3 | 200 | -0.0064 | 274.7 | 200 | 0.0011 |
| 51.1 | 0 | 0.0008 | 130.9 | 0 | 0.0079 | 210.9 | 0 | 0.0256 | 289.9 | 0 | 0.0443 |
| 51.1 | 10 | -0.0003 | 130.9 | 10 | 0.0066 | 210.9 | 10 | 0.0233 | 298.8 | 10 | 0.0392 |
| 51.1 | 20 | -0.0014 | 131.2 | 20 | 0.0054 | 211.5 | 20 | 0.0211 | 290.5 | 20 | 0.0345 |
| 50.9 | 30 | -0.0026 | 131.3 | 30 | 0.0041 | 211.8 | 30 | 0.0190 | 291.2 | 30 | 0.0305 |
| 50.8 | 40 | -0.0037 | 131.5 | 40 | 0.0028 | 211.7 | 40 | 0.0171 | 291.7 | 40 | 0.0276 |
| 50.7 | 50 | -0.0048 | 131.7 | 50 | 0.0016 | 211.9 | 50 | 0.0153 | 292.2 | 50 | 0.0251 |
| 50.7 | 60 | -0.0058 | 131.8 | 60 | 0.0005 | 212.1 | 60 | 0.0137 | 292.5 | 60 | 0.0227 |
| 50.7 | 70 | -0.0067 | 132.0 | 70 | -0.0005 | 212.2 | 70 | 0.0122 | 292.7 | 70 | 0.0206 |
| 50.7 | 80 | -0.0076 | 132.2 | 80 | -0.0015 | 212.4 | 80 | 0.0108 | 293.1 | 80 | 0.0186 |
| 50.7 | 90 | -0.0084 | 132.3 | 90 | -0.0025 | 212.6 | 90 | 0.0094 | 293.2 | 90 | 0.0168 |
| 50.7 | 100 | -0.0093 | 132.4 | 100 | -0.0034 | 212.8 | 100 | 0.0079 | 293.5 | 100 | 0.0150 |
| 50.7 | 110 | -0.0102 | 132.6 | 110 | -0.0043 | 212.7 | 110 | 0.0064 | 293.6 | 110 | 0.0133 |
| 50.7 | 120 | -0.0110 | 132.7 | 120 | -0.0052 | 212.7 | 120 | 0.0050 | 293.7 | 120 | 0.0119 |
| 50.7 | 130 | -0.0117 | 132.8 | 130 | -0.0061 | 212.9 | 130 | 0.0036 | 294.1 | 130 | 0.0104 |
| 50.7 | 140 | -0.0125 | 132.9 | 140 | $-0.0069$ | 213.0 | 140 | 0.0023 | 294.3 | 140 | 0.0090 |
| 50.7 | 150 | -0.0132 | 133.0 | 150 | -0.0077 | 213.2 | 150 | 0.0010 | 294.5 | 150 | 0.0078 |
| 50.7 | 160 | -0.0140 | 132.9 | 160 | -0.0084 | 213.5 | 160 | -0.0002 | 294.3 | 160 | 0.0064 |
| 50.7 | 170 | -0.0146 | 132.9 | 170 | -0.0092 | 213.8 | 170 | -0.0014 | 294.3 | 170 | 0.0051 |
| 50.6 | 180 | -0.0153 | 132.9 | 180 | -0.0100 | 214.0 | 180 | -0.0025 | 294.4 | 180 | 0.0040 |
| 50.7 | 190 | -0.0160 | 132.9 | 190 | $-0.0107$ | 214.3 | 190 | -0.0036 | 294.5 | 190 | 0.0028 |
| 50.8 | 200 | -0.0167 | 132.9 | 200 | $-0.0114$ | 214.4 | 200 | -0.0046 | 294.7 | 200 | 0.0016 |
| 71.4 | 0 | 0.0014 | 150.8 | 0 | 0.0112 | 230.7 | 0 | 0.0301 | 310.1 | 0 | 0.0500 |
| 71.3 | 10 | 0.0003 | 150.8 | 10 | 0.0098 | 230.6 | 10 | 0.0273 | 310.1 | 10 | 0.0437 |
| 71.5 | 20 | -0.0009 | 151.3 | 20 | 0.0084 | 231.4 | 20 | 0.0247 | 311.0 | 20 | 0.0378 |
| 71.5 | 30 | -0.0021 | 151.4 | 30 | 0.0071 | 231.8 | 30 | 0.0223 | 311.6 | 30 | 0.0335 |
| 71.5 | 40 | -0.0032 | 151.4 | 40 | 0.0057 | 231.9 | 40 | 0.0203 | 312.1 | 40 | 0.0302 |
| 71.4 | 50 | -0.0042 | 151.5 | 50 | 0.0044 | 232.0 | 50 | 0.0182 | 312.6 | 50 | 0.0273 |
| 71.4 | 60 | -0.0053 | 151.6 | 60 | 0.0032 | 232.3 | 60 | 0.0164 | 313.0 | 60 | 0.0243 |
| 71.4 | 70 | -0.0062 | 151.9 | 70 | 0.0021 | 232.4 | 70 | 0.0148 | 313.5 | 70 | 0.0221 |
| 71.5 | 80 | -0.0071 | 152.0 | 80 | 0.0010 | 232.6 | 80 | 0.0132 | 313.7 | 80 | 0.0199 |
| 71.5 | 90 | -0.0080 | 152.2 | 90 | -0.0001 | 232.9 | 90 | 0.0118 | 313.8 | 90 | 0.0180 |
| 71.5 | 100 | -0.0089 | 152.5 | 100 | -0.0011 | 232.9 | 100 | 0.0103 | 313.9 | 100 | 0.0161 |
| 71.5 | 110 | -0.0097 | 152.7 | 110 | -0.0021 | 232.9 | 110 | 0.0089 | 314.0 | 110 | 0.0143 |
| 71.4 | 120 | -0.0106 | 152.9 | 120 | -0.0031 | 232.9 | 120 | 0.0076 | 314.2 | 120 | 0.0127 |
| 71.5 | 130 | -0.0113 | 153.0 | 130 | -0.0040 | 233.1 | 130 | 0.0063 | 314.5 | 130 | 0.0111 |
| 71.5 | 140 | -0.0121 | 153.1 | 140 | -0.0048 | 233.1 | 140 | 0.0049 | 314.7 | 140 | 0.0096 |
| 71.5 | 150 | -0.0128 | 153.3 | 150 | -0.0057 | 233.3 | 150 | 0.0036 | 314.8 | 150 | 0.0081 |
| 71.5 | 160 | -0.0135 | 153.5 | 160 | -0.0065 | 233.5 | 160 | 0.0023 | 314.7 | 160 | 0.0068 |
| 71.5 | 170 | $-0.0142$ | 153.7 | 170 | -0.0073 | 233.7 | 170 | 0.0010 | 314.8 | 170 | 0.0055 |
| 71.5 | 180 | -0.0149 | 153.7 | 180 | -0.0082 | 234.0 | 180 | -0.0001 | 314.9 | 180 | 0.0042 |
| 71.5 | 190 | -0.0155 | 153.7 | 190 | -0.0090 | 234.3 | 190 | $-0.0013$ | 315.1 | 190 | 0.0029 |
| 71.4 | 200 | -0.0162 | 153.7 | 200 | -0.0098 | 234.6 | 200 | -0.0025 | 315.2 | 200 | 0.0018 |
| 91.1 | 0 | 0.0025 | 170.9 | 0 | 0.0153 | 250.4 | 0 | 0.0342 | 330.7 | 0 | 0.0570 |
| 91.2 | 10 | 0.0013 | 170.9 | 10 | 0.0136 | 250.3 | 10 | 0.0309 | 330.8 | 10 | 0.0484 |
| 91.5 | 20 | 0.0002 | 171.4 | 20 | 0.0120 | 251.2 | 20 | 0.0278 | 331.5 | 20 | 0.0403 |
| 91.6 | 30 | -0.0009 | 171.5 | 30 | 0.0104 | 251.9 | 30 | 0.0251 | 332.2 | 30 | 0.0354 |
| 91.7 | 40 | -0.0020 | 171.5 | 40 | 0.0090 | 252.1 | 40 | 0.0228 | 332.7 | 40 | 0.0315 |
| 91.6 | 50 | -0.0031 | 171.5 | 50 | 0.0075 | 252.4 | 50 | 0.0206 | 333.4 | 50 | 0.0284 |
| 91.6 | 60 | -0.0041 | 171.8 | 60 | 0.0062 | 252.5 | 60 | 0.0187 | 333.8 | 60 | 0.0255 |
| 91.8 | 70 | -0.0050 | 171.9 | 70 | 0.0049 | 252.5 | 70 | 0.0168 | 334.3 | 70 | 0.0230 |
| 91.8 | 80 | -0.0059 | 172.0 | 80 | 0.0037 | 252.6 | 80 | 0.0151 | 334.6 | 80 | 0.0207 |
| 91.8 | 90 | -0.0067 | 172.2 | 90 | 0.0025 | 252.7 | 90 | 0.0135 | 334.8 | 90 | 0.0182 |
| 91.8 | 100 | $-0.0076$ | 172.4 | 100 | 0.0014 | 253.0 | 100 | 0.0119 | 334.9 | 100 | 0.0162 |
| 91.8 | 110 | -0.0084 | 172.6 | 110 | 0.0003 | 253.1 | 110 | 0.0106 | 335.0 | 110 | 0.0142 |
| 91.9 | 120 | -0.0092 | 172.9 | 120 | -0.0008 | 253.4 | 120 | 0.0092 | 335.0 | 120 | 0.0125 |
| 91.8 | 130 | -0.0099 | 173.0 | 130 | -0.0017 | 253.6 | 130 | 0.0079 | 335.2 | 130 | 0.0108 |
| 91.8 | 140 | -0.0106 | 173.2 | 140 | -0.0028 | 253.5 | 140 | 0.0066 | 335.3 | 140 | 0.0093 |
| 91.8 | 150 | $-0.0113$ | 173.4 | 150 | -0.0038 | 253.5 | 150 | 0.0053 | 335.6 | 150 | 0.0077 |
| 91.8 | 160 | $-0.0120$ | 173.5 | 160 | -0.0047 | 253.7 | 160 | 0.0041 | 335.8 | 160 | 0.0063 |
| 91.8 | 170 | -0.0128 | 173.6 | 170 | -0.0056 | 253.8 | 170 | 0.0030 | 336.0 | 170 | 0.0049 |
| 91.8 | 180 | -0.0134 | 173.8 | 180 | -0.0064 | 254.0 | 180 | 0.0018 | 335.9 | 180 | 0.0036 |
| 91.8 | 190 | -0.0141 | 174.0 | 190 | -0.0073 | 254.1 | 190 | 0.0006 | 335.9 | 190 | 0.0023 |
| 91.9 | 200 | -0.0147 | 174.1 | 200 | -0.0081 | 254.4 | 200 | -0.0006 | 335.9 | 200 | 0.0010 |



Figure 2. Isobars for fullerites. From top to bottom, 10, 50, 100,150 , and 200 MPa .


Figure 3. Comparison of isothermal compressibility of fullerites (bottom two curves with open squares for $250^{\circ} \mathrm{C}$ and filled squares for $50^{\circ} \mathrm{C}$ ) and graphite (top two curves with open circles for $250^{\circ} \mathrm{C}$ and filled circles for $50^{\circ} \mathrm{C}$ ).

Figure 2 indicate considerable compressibility and thermal expansion. These results are measured isothermally starting at low temperatures. Compressibility is found to be reversible; i.e., after reducing pressure at each temperature, the specific volume is restored to its initial low-pressure value. Thismeans that the major contribution to the compressibility is from the material, not from possible porosity.

Within the temperature range of $40-340^{\circ} \mathrm{C}$, there is no significant phase transition found at both ambient pressure and 200 MPa . Thermal expansion at each pressure shows an almost linear increase, as demonstrated in Figure 2.

Figure 3 presents a comparison of two isotherms for fullerites and graphite with the same scales for the $y$ axes. Fullerites are much more compressible than graphite ( $\Delta V=$ -0.018 versus $-0.011 \mathrm{~cm}^{3} . \mathrm{g}^{-1}$ at $50^{\circ} \mathrm{C}$ and -0.035 versus -0.018 $\mathrm{cm}^{3} \mathrm{~g}^{-1}$ at $250^{\circ} \mathrm{C}$, respectively). Also, there is a large difference in thermal expansion. For example, for fullerites, the volume expansion is $+0.031 \mathrm{~cm}^{3} \cdot \mathrm{~g}^{-1}$ in going from 50 to $200^{\circ} \mathrm{C}$ at 10 MPa. By contrast, the corresponding expansion for graphite is only $+0.007 \mathrm{~cm}^{3} \cdot \mathrm{~g}^{-1}$. A few average compressibility ( $\beta$ ) and

Table 2. Compressibility and Thermal Expansion of Fullerites and Graphite

|  | $\alpha / \mathrm{K}^{-1}\left(50-250^{\circ} \mathrm{C}\right)$ |  |  | $\beta / \mathrm{MPa}^{-1}(0-200 \mathrm{MPa})$ |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | $P=0.1 \mathrm{MPa}$ | $P=200 \mathrm{MPa}$ |  | $t=50^{\circ} \mathrm{C}$ | $t=250^{\circ} \mathrm{C}$ |
| fullerites | $2.7 \times 10^{-4}$ | $1.3 \times 10^{-4}$ |  | $1.4 \times 10^{-4}$ | $2.6 \times 10^{-4}$ |
| graphite | $0.9 \times 10^{-4}$ | $0.2 \times 10^{-4}$ |  | $1.2 \times 10^{-4}$ | $1.9 \times 10^{-4}$ |

thermal expansion ( $\alpha$ ) values are given in Table 2. They are calculated from the following formulas:

$$
\begin{align*}
& \alpha=\frac{1}{V_{0}}\left(\frac{\Delta V}{\Delta T}\right)_{\mathrm{P}}  \tag{1}\\
& \beta=\frac{1}{V_{0}}\left(\frac{\Delta V}{\Delta P}\right)_{\mathrm{T}} \tag{2}
\end{align*}
$$

A previous study suggests that fullerites are extremely hard (4). We find that this can only be true to extremely high pressures. At low and moderate pressures (up to several hundred megapascals), the free volumes between the carbon cages should contribute tremendous compressibility and thermal expansion, as shown in our data.

## Conclusions

On the basis of specific volumes for $\mathrm{C}_{60} / \mathrm{C}_{70}$ (3:1) fullerites and graphite, measured up to $340^{\circ} \mathrm{C}$ and 200 MPa , fullerite compressibilities and thermal expansions are found to be much higher than those of graphite. While graphite exhibits little isobaric thermal expansion at pressures above 10 MPa , fullerites exhibit significant and monotonic expansion. This is consistent with a lower degree of molecular and supermolecular packing in fullerites compared to graphite.

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